# SEMIPARAMETRIC MODELING OF CONSUMER PRICE INDEX

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**Abstract.** Many classical data, for example, exchange rate, stock price, and consumer price index (CPI) data cannot be analyzed under independent observation assumption. In addition, some time series data cannot be modeled well into a fully linear model, for instance, CPI, price of raw materials for some certain industries and price of some industrial products data in which monetary crisis of Indonesia in 1998 has caused a dramatic effect on the time series of CPI, price of raw materials and industrial products. A semiparametric model is a mixture model between parametric and nonparametric models. If we apply it to time series data, we will obtain a semiparametric time series model known as partly linear autoregressive model:

$$y_t = \beta \ y_{t-1} + g(y_{t-2}, ..., y_{t-p}) + \varepsilon_t \text{ for } t \ge p+1.$$

Here  $\beta$  is an unknown parameter to be estimated, g(.) is an unknown function in  $R^{p-1}$ ,  $\varepsilon_t$  are i.i.d. random errors with  $E(\varepsilon_1)=0$  and  $E(\varepsilon_1^2)<\infty$ , and  $\varepsilon_t$  are independent of  $y_s$  for all s=1,2,...,p and  $t\geq p+1$ . Based on the model above, we investigate a model for general consumer price index (GCPI) of Jember data recorded monthly from January 1998 to December 2002 by Statistic Center Bureau of Jember.

Keywords: Least Square Estimator, Kernel Estimator, Semiparametric Model,

Consumer Price Index

MSC 2020: 62F99

#### 1. Introduction

In last twenty years, many authors have shown interest in semiparametric regression models, especially, partly linear regression models,  $y_j = x_j' \beta + g(t_j) + \varepsilon_j$  for j = 1,2,...; e.g. Ansley and Wecker (1983), Heckman (1986), Rice (1986), Chen (1988), Chen and Shiau (1991), and Andrews (1991) investigated asymptotic behaviors by using spline smoothing techniques and Robinson (1988), Speackman (1988), Gao (1992), and Gao, et al (1994) also obtained some asymptotic results by using kernel or nearest neighbor smoothing under the case where the  $(x_j, t_j)$  are i.i.d. random variables or fixed design points, and Wahba (1990), Budiantara (1999) and Hardle (2000) studied partly linear model for independent observations case. However, many classical data, for example, exchange rate data, stock price data, and consumer price index data, cannot be analyzed under independent observation assumption. In addition, some time series data cannot be

modeled as a fully linear model, for instance, consumer price index (CPI) data recorded monthly from January 1998 to December 2002 by Statistic Center Bureau of Jember in which monetary crisis of Indonesia in 1998 has caused a dramatic effect on the time series of CPI. Lestari (2001), Lestari (2003), Lestari (2004), and Lestari (2005) studied estimation, asymptotic normality and iterated logarithm distribution of partly linear autoregressive estimators; and applied partly linear autoregressive model to the consumer price index of Jember data. Beside that, latest development in the semiparametric regression has given a strong foundation to semiparametric time series analysis.

The important thing is how we analyze and apply semiparametric regression model to time series data. The resulting model is known as partly linear autoregressive model given by:

$$y_{t} = \beta \ y_{t-1} + g(y_{t-2}, \dots, y_{t-n}) + \varepsilon_{t}, \ t \ge p+1$$
 (1)

where  $\beta$  is an unknown parameter to be estimated, g(.) is an unknown function in  $R^{p-1}$ ,  $\varepsilon_t$  are i.i.d. random errors with  $E(\varepsilon_1) = 0$  and  $E(\varepsilon_1^2) < \infty$ , and  $\varepsilon_t$  are independent of  $\gamma_s$ for all s = 1, 2, ..., p.

In this paper, we investigate a semiparametric time series model for the general consumer price index (GCPI) of Jember data which is known as partly linear autoregressive model.

## 2. Methodology

The model (1) contains unknown parameter  $\beta$  and unknown function g(.) to be estimated. Least square method is used to obtain estimator  $\hat{\beta}_T$  of  $\beta$ . The estimate of g(.) can be obtained by using kernel estimator approach. In association with the GCPI data, of course, Firstly we identify the parametric and nonparametric components of data. Secondly, we determine an optimum bandwidth for kernel estimator approach with generalized cross validation (GCV) criterion and Gaussian kernel function. Finally, we estimate the model of GCPI by investigating and comparing their mean square errors (MSE), errors and plot for three models approach, i.e., linear autoregressive model, ARIMA model, and partly linear autoregressive model. For estimating and plotting, we use MINITAB, S-PLUS, and MATLAB programs.

#### 3. Results

#### 3. 1. Estimation of Function g(.) and Parameter $\beta$

Assume that  $\{y_t, t = p+1, p+2,..., T\}$  satisfy the partly linear autoregressive model :

$$y_t = \beta y_{t-1} + g(y_{t-2}, ..., y_{t-p}) + \varepsilon_t, t \ge p+1.$$
 (2)

Then, we have:

$$g(y_{t-2},...,y_{t-p}) = E((y_t - \beta y_{t-1}) | y_{t-2},...,y_{t-p})$$

$$= E(y_t | y_{t-2},...,y_{t-p}) - \beta E(y_{t-1} | y_{t-2},...,y_{t-p})$$

$$= g_1(y_{t-2},...,y_{t-p}) - \beta g_2(y_{t-2},...,y_{t-p}) \text{ (say)}$$
(3)

Hence, the natural estimates of  $g_1(.)$ ,  $g_2(.)$  and g(.) of (3) can be obtained by using kernel estimator approach defined by :

$$\hat{g}_{1T}(x_t) = \sum_{s=p+1}^{T} W_{Ts}(x_t) y_s,$$
(4)

$$\hat{g}_{2T}(x_t) = \sum_{s=p+1}^{T} W_{Ts}(x_t) y_{s-1}, \tag{5}$$

and

$$\hat{g}_{T}(x_{t}) = \hat{g}_{1T}(x_{t}) - \beta \hat{g}_{2T}(x_{t}) \tag{6}$$

where  $x_t = (y_{t-2},...,y_{t-p})$  and  $W_{ts}(.)$  are kernel weight function Nadaraya-Watson given by :

$$W_{Ts}(x) = K((x - x_s)/h) / \sum_{t=p+1}^{T} K((x - x_t)/h)$$
 (7)

where  $K: \mathbb{R}^{p-1} \to \mathbb{R}$  is a function and  $\{h = h_T; T > p\}$  is a sequence of nonnegative real numbers.

Now, based on the model  $y_t = \beta y_{t-1} + \hat{g}_T(y_{t-2},....,y_{t-p}) + \varepsilon_t$ , t = p+1,...,T, we have the least square estimator  $\hat{\beta}_T$  of  $\beta$ :

$$\hat{\beta}_{T} = \frac{\sum_{t=p+1}^{T} (y_{t-1} - \hat{g}_{2T}(y_{t-2}, ..., y_{t-p}))(y_{t} - \hat{g}_{1T}(y_{t-2}, ..., y_{t-p}))}{\sum_{t=p+1}^{T} (y_{t-1} - \hat{g}_{2T}(y_{t-2}, ..., y_{t-p}))^{2}}$$
(8)

#### 3.2. Investigation of GCPI Model.

Based on the model (1), we investigate a model for general consumer price index (GCPI) data recorded monthly from January 1998 to December 2002 by Statistic Center Bureau of Jember. The GCPI data and their series plot are shown in Table 1 and Figure 1,

respectively.

Table 1. General consumer price index from january 1998 to december 2001

Year	GCPI								
1998	183.69	1999	187.8	2000	196.99	2001	198	2002	218.92
	185.86		188.01		197.12		199.87		217.1
	186.65		190.45		197.23		197.28		210.27
	192.55		193.1		197.29		199.67		218.07
	195.14		194.25		197.37		198.83		219.48
	194.77		192.35		197.4		199.54		219.96
	193.35		193.5		197.5		199.79		218.88
	192.75		195.2		197.73		199.92		216.89
	193.1		196.37		197.76		200.21		210.09
	189.92		195.88		197.84		218.09		216.25
	188.1		198.22		197.9		219.28		215.59
	186.69		196.41		197.95		220		219.06

Source: Statistic Center Bureau of Jember

#### 3.2.1. Autoregressive Model Approach

In this approach, we consider a linear model as follows:

$$y_{t} = \beta_{0} + \beta_{1} y_{t-1} + \beta_{2} y_{t-2} + \dots + \beta_{p} y_{t-p} + \varepsilon_{t}.$$

$$(9)$$

The linear regression analysis result on the data gives an estimated model:

$$\hat{y}_t = 8.81 + 0.923y_{t-1} + 0.036y_{t-2} \tag{10}$$

Validation result of  $\hat{\beta}_0$ ,  $\hat{\beta}_1$  and  $\hat{\beta}_2$  shows that  $\hat{\beta}_1$  is significant, and  $\hat{\beta}_0$  and  $\hat{\beta}_2$  are not significant. Plot between  $y_t$  and  $\hat{y}_t$  is shown in Figure 2.

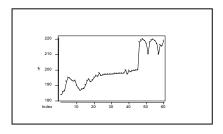


Figure 1. Series Plot of GCPI Data

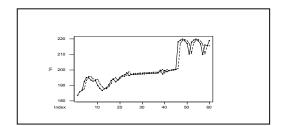
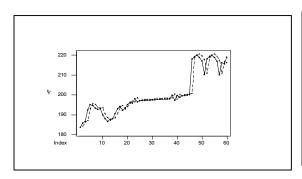


Figure 2. Plot Between  $y_t(-)$  and  $\hat{y}_t = 8.81 + 0.923 y_{t-1} + 0.036 y_{t-2}$  (---)

In addition, plotting of residuals as shown model (10) shows that there are a right skew, outliers and indicates no normal distribution. Next, by getting out variables with no significant coefficients from the model, we obtain:

$$y_{t} = 1.00287 y_{t-1} + \varepsilon_{t} \tag{11}$$

Plotting of residuals model (11) shows that there are a right skew, outliers and indicates no normal distribution. Plot between  $y_t$  and  $\hat{y}_t = 1.00287 y_{t-1}$  is shown in Figure 3. Residuals plots for models (10) and (11) are shown in Figure 4 and Figure 5, respectively.



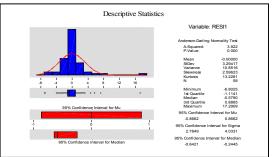
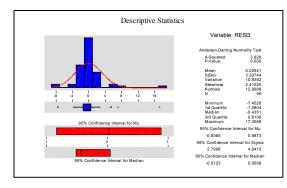


Figure 3. Plot between  $y_t$  and  $\hat{y}_t = 1.00287 y_{t-1}$  Figure 4. Residuals plot for Model (10)

### 3.2.2. ARIMA Model Approach

Figure 1 shows a series with trend. It means that the series has not been stationary yet. Next, by using difference d = 1, i.e.,  $w_t = y_t - y_{t-1}$ , we have series plot of  $w_t$  as shown in Figure 6. Figure 6 shows that data has been stationary. Based on the autocorrelation function (ACF) and partial autocorrelation function (PACF) plots in which they cut off after lag 5 and lag 6, we have the estimated model of **ARIMA(1,1,0)(1,0,0)**<sup>6</sup>



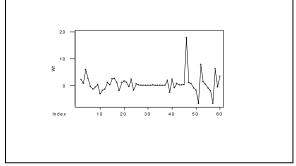


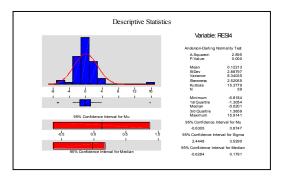
Figure 5. Residuals plot for model (11)

Figure 6. Series plot with difference d = 1

Although diagnostic checking result shows that residuals has been white noise but estimation of parameters result shows that SAR parameter is significant different from zero and AR parameter is not significant. Plot of residuals normality shows that residuals are not normal and have outliers as shown in Figure 7.

#### 3.2.3. Semiparametric Model Approach

By plotting between  $y_t$  and  $y_{t-1}$ ; and between  $y_t$  and  $y_{t-2}$  we knew that plotting result between  $y_t$  and  $y_{t-1}$  was relatively linear (Figure 8). On the other hand, plotting result between  $y_t$  and  $y_{t-2}$  was not linear and had no certain pattern (Figure 9). Therefore,  $y_{t-1}$  and  $y_{t-2}$  were as parametric and nonparametric components, respectively.



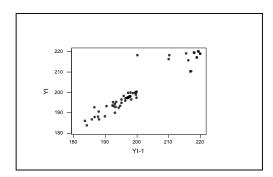


Figure 7. Residuals plot for ARIMA Model

Figure 8. Plot between  $y_t$  and  $y_{t-1}$ 

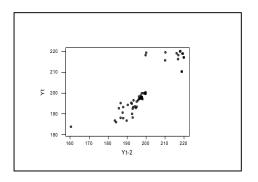
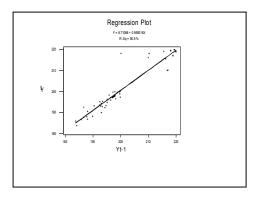


Figure 9. Plot between  $y_t$  and  $y_{t-2}$ 

It is also supported by linear regression plot results between  $y_t$  and  $y_{t-1}$  with  $R^2 = 90.6$  %, and between  $y_t$  and  $y_{t-2}$  with  $R^2 = 78.6$  % as shown in Figure 10 and Figure 11, respectively.



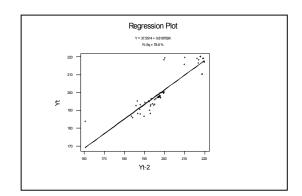


Figure 10. Regression plot between  $y_t$  and  $y_{t-1}$  Figure 11. Regression plot between  $y_t$  and  $y_{t-2}$ 

After determining both parametric and nonparametric components, we find the optimum bandwidth for Gaussian kernel estimator approach with the generalized cross validation (GCV) criterion. So that, by using programs Matlab and Minitab, we obtained some bandwidth and GCV values as shown in Table 2 and Figure 12, respectively. Table 2 and

Figure 12 show that the optimum bandwidth is 0.017, because GCV minimum, i.e. 1.8447, is obtained at bandwidth (h) = 0.017.

Next, based on that optimum bandwidth we estimated  $\hat{g}_T(y_{t-2})$ ,  $\hat{\beta}_T$ ,  $\hat{y}_t$  and  $\varepsilon_t$  values by using program Matlab. We got  $\hat{\beta}_T = 0.9192$ ; and  $\hat{y}_t$ ,  $\hat{g}_T(y_{t-2})$  and  $\varepsilon_t$  as shown in Table 3. It shows that errors are relatively small or leads to zero for every t. So, we obtained the mean square error (MSE), i.e., 0.007083. The relationship of  $\hat{y}_t$ ,  $y_{t-1}$  and  $y_{t-2}$  formed a surface as shown in Figure 13.

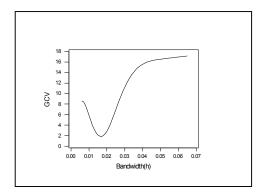


Figure 12. GCV versus bandwidth plot

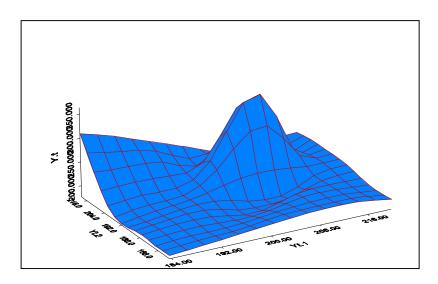


Figure 13. Surface performed by  $\hat{y}_t$ ,  $y_{t-1}$  and  $y_{t-2}$ 

Next, based on that optimum bandwidth we estimated  $\hat{g}_T(y_{t-2})$ ,  $\hat{\beta}_T$ ,  $\hat{y}_t$  and  $\varepsilon_t$  values by using program Matlab. We got  $\hat{\beta}_T = 0.9192$ ; and  $\hat{y}_t$ ,  $\hat{g}_T(y_{t-2})$  and  $\varepsilon_t$  as shown in Table 3. It shows that errors are relatively small or leads to zero for every t. So, we obtained the mean square error (MSE), i.e., 0.007083. The relationship of  $\hat{y}_t$ ,  $y_{t-1}$  and  $y_{t-2}$  formed a surface as shown in Figure 13.

Table 2. Some GCV values for some bandwidths

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	Bandwidth	GCV	Bandwidth	GCV
	0.01	5.83	0.017	1.8447
	0.011	4.8474	0.018	1.9758
	0.012	3.9612	0.019	2.3006
	0.013	3.2064	0.02	2.8035
	0.014	2.6038	0.021	3.4589
	0.015	2.1676	0.022	4.2347
	0.016	1.9107	0.023	5.0963

Table 3. Estimated values of  $\hat{y}_t$ ,  $\hat{g}_T(y_{t-2})$  and  $\varepsilon_t$ 

$\begin{array}{ c c c c c c c c }\hline No & \hat{y}_t & \hat{g}_T(y_{t-2}) & \varepsilon_t & No & \hat{y}_t & \hat{g}_T(y_{t-2}) & \varepsilon_t \\\hline 1 & 183.685 & 14.3408 & 0 & 31 & 197.519 & 16.0686 & -0.024 \\ 2 & 185.855 & 17.0072 & 0 & 32 & 197.701 & 16.1586 & 0.024 \\ 3 & 186.645 & 15.8024 & 0 & 33 & 197.755 & 16.0012 & 0 \\ 4 & 192.545 & 20.9762 & 0 & 34 & 197.832 & 16.0513 & 0.0024 \\ 5 & 194.972 & 17.9796 & 0.1632 & 35 & 197.897 & 16.0425 & -0.0024 \\ 6 & 194.765 & 15.392 & 0 & 36 & 197.945 & 16.035 & 0 \\ 7 & 193.347 & 14.3142 & -0.0021 & 37 & 198.018 & 16.0627 & -0.0238 \\ 8 & 192.745 & 15.0174 & 0 & 38 & 199.786 & 17.784 & 0.079 \\ 9 & 193.095 & 15.919 & 0 & 39 & 197.331 & 13.6103 & -0.0563 \\ 10 & 189.915 & 12.4172 & 0 & 40 & 199.87 & 18.5302 & -0.2053 \\ 11 & 188.23 & 13.6553 & -0.1349 & 41 & 199.14 & 15.6035 & -0.3156 \\ 12 & 186.685 & 13.7834 & 0 & 42 & 199.535 & 16.7701 & 0 \\ 13 & 187.795 & 16.1895 & 0 & 43 & 199.785 & 16.3674 & 0 \\ 14 & 188.168 & 15.5424 & -0.1632 & 44 & 199.915 & 16.2676 & 0 \\ 15 & 190.445 & 17.6261 & 0 & 45 & 200.205 & 16.4381 & 0 \\ 16 & 193.095 & 18.0332 & 0 & 46 & 217.879 & 33.8462 & 0.2053 \\ 17 & 194.245 & 16.7472 & 0 & 47 & 219.274 & 18.8057 & 0 \\ 18 & 192.21 & 13.6553 & 0.1349 & 48 & 219.919 & 18.3572 & 0.0747 \\ 19 & 193.495 & 16.6867 & 0 & 49 & 218.914 & 16.69 & 0 \\ 20 & 195.195 & 17.3295 & 0 & 50 & 217.084 & 15.8526 & 0.0102 \\ 21 & 196.365 & 16.9369 & 0 & 51 & 210.265 & 10.7066 & -0.0008 \\ 22 & 195.873 & 15.3693 & 0.0021 & 52 & 218.064 & 24.7841 & 0 \\ 24 & 196.405 & 14.2008 & 0 & 54 & 220.029 & 18.2827 & -0.0747 \\ 25 & 196.985 & 16.4446 & 0 & 55 & 218.874 & 16.6868 & 0 \\ 26 & 197.24 & 16.1667 & -0.1252 & 56 & 216.894 & 15.6998 & -0.0102 \\ 27 & 197.225 & 16.0319 & 0 & 57 & 210.083 & 10.7181 & 0.0008 \\ 28 & 197.285 & 15.9908 & 0 & 58 & 216.244 & 23.1296 & 0 \\ 29 & 197.355 & 16.0061 & 0.0096 & 59 & 215.584 & 16.8071 & 0 \\ 30 & 197.082 & 15.6599 & 0.3122 & 60 & 219.054 & 20.8838 & 0 \\ \end{array}$					•	1,0101-2)	ı	
2       185.855       17.0072       0       32       197.701       16.1586       0.024         3       186.645       15.8024       0       33       197.755       16.0012       0         4       192.545       20.9762       0       34       197.832       16.0513       0.0024         5       194.972       17.9796       0.1632       35       197.897       16.0425       -0.0024         6       194.765       15.392       0       36       197.945       16.035       0         7       193.347       14.3142       -0.0021       37       198.018       16.0627       -0.0238         8       192.745       15.0174       0       38       199.786       17.784       0.079         9       193.095       15.919       0       39       197.331       13.6103       -0.0563         10       189.915       12.4172       0       40       199.87       18.5302       -0.2053         11       188.23       13.6553       -0.1349       41       199.14       15.6035       -0.3156         12       186.685       13.7834       0       42       199.535       16.7701       0 <th>No</th> <th><math>\hat{{\mathcal{Y}}}_t</math></th> <th><math>\hat{g}_T(y_{t-2})</math></th> <th><math>\mathcal{E}_t</math></th> <th>No</th> <th><math>\hat{\boldsymbol{\mathcal{Y}}}_t</math></th> <th><math>\hat{g}_{T}(y_{t-2})</math></th> <th><math>\mathcal{E}_t</math></th>	No	$\hat{{\mathcal{Y}}}_t$	$\hat{g}_T(y_{t-2})$	$\mathcal{E}_t$	No	$\hat{\boldsymbol{\mathcal{Y}}}_t$	$\hat{g}_{T}(y_{t-2})$	$\mathcal{E}_t$
3         186.645         15.8024         0         33         197.755         16.0012         0           4         192.545         20.9762         0         34         197.832         16.0513         0.0024           5         194.972         17.9796         0.1632         35         197.897         16.0425         -0.0024           6         194.765         15.392         0         36         197.945         16.035         0           7         193.347         14.3142         -0.0021         37         198.018         16.0627         -0.0238           8         192.745         15.0174         0         38         199.786         17.784         0.079           9         193.095         15.919         0         39         197.331         13.6103         -0.0563           10         189.915         12.4172         0         40         199.87         18.5302         -0.2053           11         188.23         13.6553         -0.1349         41         199.14         15.6035         -0.3156           12         186.685         13.7834         0         42         199.535         16.3674         0           14	1	183.685	14.3408	0	31	197.519	16.0686	-0.024
4         192.545         20.9762         0         34         197.832         16.0513         0.0024           5         194.972         17.9796         0.1632         35         197.897         16.0425         -0.0024           6         194.765         15.392         0         36         197.945         16.035         0           7         193.347         14.3142         -0.0021         37         198.018         16.0627         -0.0238           8         192.745         15.0174         0         38         199.786         17.784         0.079           9         193.095         15.919         0         39         197.331         13.6103         -0.0563           10         189.915         12.4172         0         40         199.87         18.5302         -0.2053           11         188.23         13.6553         -0.1349         41         199.14         15.6035         -0.3156           12         186.685         13.7834         0         42         199.535         16.7701         0           13         187.795         16.1895         0         43         199.785         16.3674         0           14	2	185.855	17.0072	0	32	197.701	16.1586	0.024
5         194.972         17.9796         0.1632         35         197.897         16.0425         -0.0024           6         194.765         15.392         0         36         197.945         16.035         0           7         193.347         14.3142         -0.0021         37         198.018         16.0627         -0.0238           8         192.745         15.0174         0         38         199.786         17.784         0.079           9         193.095         15.919         0         39         197.331         13.6103         -0.0563           10         189.915         12.4172         0         40         199.87         18.5302         -0.2053           11         188.23         13.6553         -0.1349         41         199.14         15.6035         -0.3156           12         186.685         13.7834         0         42         199.535         16.7701         0           13         187.795         16.1895         0         43         199.785         16.3674         0           14         188.168         15.5424         -0.1632         44         199.915         16.2676         0           15	3	186.645	15.8024	0	33	197.755	16.0012	0
6         194.765         15.392         0         36         197.945         16.035         0           7         193.347         14.3142         -0.0021         37         198.018         16.0627         -0.0238           8         192.745         15.0174         0         38         199.786         17.784         0.079           9         193.095         15.919         0         39         197.331         13.6103         -0.0563           10         189.915         12.4172         0         40         199.87         18.5302         -0.2053           11         188.23         13.6553         -0.1349         41         199.14         15.6035         -0.3156           12         186.685         13.7834         0         42         199.535         16.7701         0           13         187.795         16.1895         0         43         199.785         16.3674         0           14         188.168         15.5424         -0.1632         44         199.915         16.2676         0           15         190.445         17.6261         0         45         200.205         16.4381         0           16 <t< td=""><td>4</td><td>192.545</td><td>20.9762</td><td>0</td><td>34</td><td>197.832</td><td>16.0513</td><td>0.0024</td></t<>	4	192.545	20.9762	0	34	197.832	16.0513	0.0024
7       193.347       14.3142       -0.0021       37       198.018       16.0627       -0.0238         8       192.745       15.0174       0       38       199.786       17.784       0.079         9       193.095       15.919       0       39       197.331       13.6103       -0.0563         10       189.915       12.4172       0       40       199.87       18.5302       -0.2053         11       188.23       13.6553       -0.1349       41       199.14       15.6035       -0.3156         12       186.685       13.7834       0       42       199.535       16.7701       0         13       187.795       16.1895       0       43       199.785       16.3674       0         14       188.168       15.5424       -0.1632       44       199.915       16.2676       0         15       190.445       17.6261       0       45       200.205       16.4381       0         16       193.095       18.0332       0       46       217.879       33.8462       0.2053         17       194.245       16.7472       0       47       219.274       18.8057       0	5	194.972	17.9796	0.1632	35	197.897	16.0425	-0.0024
8       192.745       15.0174       0       38       199.786       17.784       0.079         9       193.095       15.919       0       39       197.331       13.6103       -0.0563         10       189.915       12.4172       0       40       199.87       18.5302       -0.2053         11       188.23       13.6553       -0.1349       41       199.14       15.6035       -0.3156         12       186.685       13.7834       0       42       199.535       16.7701       0         13       187.795       16.1895       0       43       199.785       16.3674       0         14       188.168       15.5424       -0.1632       44       199.915       16.2676       0         15       190.445       17.6261       0       45       200.205       16.4381       0         16       193.095       18.0332       0       46       217.879       33.8462       0.2053         17       194.245       16.7472       0       47       219.274       18.8057       0         18       192.21       13.6553       0.1349       48       219.919       18.3572       0.0747	6	194.765	15.392	0	36	197.945	16.035	0
9       193.095       15.919       0       39       197.331       13.6103       -0.0563         10       189.915       12.4172       0       40       199.87       18.5302       -0.2053         11       188.23       13.6553       -0.1349       41       199.14       15.6035       -0.3156         12       186.685       13.7834       0       42       199.535       16.7701       0         13       187.795       16.1895       0       43       199.785       16.3674       0         14       188.168       15.5424       -0.1632       44       199.915       16.2676       0         15       190.445       17.6261       0       45       200.205       16.4381       0         16       193.095       18.0332       0       46       217.879       33.8462       0.2053         17       194.245       16.7472       0       47       219.274       18.8057       0         18       192.21       13.6553       0.1349       48       219.919       18.3572       0.0747         19       193.495       16.6867       0       49       218.914       16.69       0 <t< td=""><td>7</td><td>193.347</td><td>14.3142</td><td>-0.0021</td><td>37</td><td>198.018</td><td>16.0627</td><td>-0.0238</td></t<>	7	193.347	14.3142	-0.0021	37	198.018	16.0627	-0.0238
10         189.915         12.4172         0         40         199.87         18.5302         -0.2053           11         188.23         13.6553         -0.1349         41         199.14         15.6035         -0.3156           12         186.685         13.7834         0         42         199.535         16.7701         0           13         187.795         16.1895         0         43         199.785         16.3674         0           14         188.168         15.5424         -0.1632         44         199.915         16.2676         0           15         190.445         17.6261         0         45         200.205         16.4381         0           16         193.095         18.0332         0         46         217.879         33.8462         0.2053           17         194.245         16.7472         0         47         219.274         18.8057         0           18         192.21         13.6553         0.1349         48         219.919         18.3572         0.0747           19         193.495         16.6867         0         49         218.914         16.69         0           20	8	192.745	15.0174	0	38	199.786	17.784	0.079
11       188.23       13.6553       -0.1349       41       199.14       15.6035       -0.3156         12       186.685       13.7834       0       42       199.535       16.7701       0         13       187.795       16.1895       0       43       199.785       16.3674       0         14       188.168       15.5424       -0.1632       44       199.915       16.2676       0         15       190.445       17.6261       0       45       200.205       16.4381       0         16       193.095       18.0332       0       46       217.879       33.8462       0.2053         17       194.245       16.7472       0       47       219.274       18.8057       0         18       192.21       13.6553       0.1349       48       219.919       18.3572       0.0747         19       193.495       16.6867       0       49       218.914       16.69       0         20       195.195       17.3295       0       50       217.084       15.8526       0.0102         21       196.365       16.9369       0       51       210.265       10.7066       -0.0008	9	193.095	15.919	0	39	197.331	13.6103	-0.0563
12       186.685       13.7834       0       42       199.535       16.7701       0         13       187.795       16.1895       0       43       199.785       16.3674       0         14       188.168       15.5424       -0.1632       44       199.915       16.2676       0         15       190.445       17.6261       0       45       200.205       16.4381       0         16       193.095       18.0332       0       46       217.879       33.8462       0.2053         17       194.245       16.7472       0       47       219.274       18.8057       0         18       192.21       13.6553       0.1349       48       219.919       18.3572       0.0747         19       193.495       16.6867       0       49       218.914       16.69       0         20       195.195       17.3295       0       50       217.084       15.8526       0.0102         21       196.365       16.9369       0       51       210.265       10.7066       -0.0008         22       195.873       15.3693       0.0021       52       218.064       24.7841       0	10	189.915	12.4172	0	40	199.87	18.5302	-0.2053
13     187.795     16.1895     0     43     199.785     16.3674     0       14     188.168     15.5424     -0.1632     44     199.915     16.2676     0       15     190.445     17.6261     0     45     200.205     16.4381     0       16     193.095     18.0332     0     46     217.879     33.8462     0.2053       17     194.245     16.7472     0     47     219.274     18.8057     0       18     192.21     13.6553     0.1349     48     219.919     18.3572     0.0747       19     193.495     16.6867     0     49     218.914     16.69     0       20     195.195     17.3295     0     50     217.084     15.8526     0.0102       21     196.365     16.9369     0     51     210.265     10.7066     -0.0008       22     195.873     15.3693     0.0021     52     218.064     24.7841     0       23     198.089     18.0365     0.1252     53     219.474     19.0241     0       24     196.405     14.2008     0     54     220.029     18.2827     -0.0747       25     196.985     16.4446	11	188.23	13.6553	-0.1349	41	199.14	15.6035	-0.3156
14       188.168       15.5424       -0.1632       44       199.915       16.2676       0         15       190.445       17.6261       0       45       200.205       16.4381       0         16       193.095       18.0332       0       46       217.879       33.8462       0.2053         17       194.245       16.7472       0       47       219.274       18.8057       0         18       192.21       13.6553       0.1349       48       219.919       18.3572       0.0747         19       193.495       16.6867       0       49       218.914       16.69       0         20       195.195       17.3295       0       50       217.084       15.8526       0.0102         21       196.365       16.9369       0       51       210.265       10.7066       -0.0008         22       195.873       15.3693       0.0021       52       218.064       24.7841       0         23       198.089       18.0365       0.1252       53       219.474       19.0241       0         24       196.405       14.2008       0       54       220.029       18.2827       -0.0747 <td>12</td> <td>186.685</td> <td>13.7834</td> <td>0</td> <td>42</td> <td>199.535</td> <td>16.7701</td> <td>0</td>	12	186.685	13.7834	0	42	199.535	16.7701	0
15       190.445       17.6261       0       45       200.205       16.4381       0         16       193.095       18.0332       0       46       217.879       33.8462       0.2053         17       194.245       16.7472       0       47       219.274       18.8057       0         18       192.21       13.6553       0.1349       48       219.919       18.3572       0.0747         19       193.495       16.6867       0       49       218.914       16.69       0         20       195.195       17.3295       0       50       217.084       15.8526       0.0102         21       196.365       16.9369       0       51       210.265       10.7066       -0.0008         22       195.873       15.3693       0.0021       52       218.064       24.7841       0         23       198.089       18.0365       0.1252       53       219.474       19.0241       0         24       196.405       14.2008       0       54       220.029       18.2827       -0.0747         25       196.985       16.4446       0       55       218.874       16.6868       0	13	187.795	16.1895	0	43	199.785	16.3674	0
16       193.095       18.0332       0       46       217.879       33.8462       0.2053         17       194.245       16.7472       0       47       219.274       18.8057       0         18       192.21       13.6553       0.1349       48       219.919       18.3572       0.0747         19       193.495       16.6867       0       49       218.914       16.69       0         20       195.195       17.3295       0       50       217.084       15.8526       0.0102         21       196.365       16.9369       0       51       210.265       10.7066       -0.0008         22       195.873       15.3693       0.0021       52       218.064       24.7841       0         23       198.089       18.0365       0.1252       53       219.474       19.0241       0         24       196.405       14.2008       0       54       220.029       18.2827       -0.0747         25       196.985       16.4446       0       55       218.874       16.6868       0         26       197.24       16.1667       -0.1252       56       216.894       15.6998       -0.0102	14	188.168	15.5424	-0.1632	44	199.915	16.2676	0
17     194.245     16.7472     0     47     219.274     18.8057     0       18     192.21     13.6553     0.1349     48     219.919     18.3572     0.0747       19     193.495     16.6867     0     49     218.914     16.69     0       20     195.195     17.3295     0     50     217.084     15.8526     0.0102       21     196.365     16.9369     0     51     210.265     10.7066     -0.0008       22     195.873     15.3693     0.0021     52     218.064     24.7841     0       23     198.089     18.0365     0.1252     53     219.474     19.0241     0       24     196.405     14.2008     0     54     220.029     18.2827     -0.0747       25     196.985     16.4446     0     55     218.874     16.6868     0       26     197.24     16.1667     -0.1252     56     216.894     15.6998     -0.0102       27     197.225     16.0319     0     57     210.083     10.7181     0.0008       28     197.285     15.9908     0     58     216.244     23.1296     0       29     197.355     16.0061 <td>15</td> <td>190.445</td> <td>17.6261</td> <td>0</td> <td>45</td> <td>200.205</td> <td>16.4381</td> <td>0</td>	15	190.445	17.6261	0	45	200.205	16.4381	0
18     192.21     13.6553     0.1349     48     219.919     18.3572     0.0747       19     193.495     16.6867     0     49     218.914     16.69     0       20     195.195     17.3295     0     50     217.084     15.8526     0.0102       21     196.365     16.9369     0     51     210.265     10.7066     -0.0008       22     195.873     15.3693     0.0021     52     218.064     24.7841     0       23     198.089     18.0365     0.1252     53     219.474     19.0241     0       24     196.405     14.2008     0     54     220.029     18.2827     -0.0747       25     196.985     16.4446     0     55     218.874     16.6868     0       26     197.24     16.1667     -0.1252     56     216.894     15.6998     -0.0102       27     197.225     16.0319     0     57     210.083     10.7181     0.0008       28     197.285     15.9908     0     58     216.244     23.1296     0       29     197.355     16.0061     0.0096     59     215.584     16.8071     0	16	193.095	18.0332	0	46	217.879	33.8462	0.2053
19     193.495     16.6867     0     49     218.914     16.69     0       20     195.195     17.3295     0     50     217.084     15.8526     0.0102       21     196.365     16.9369     0     51     210.265     10.7066     -0.0008       22     195.873     15.3693     0.0021     52     218.064     24.7841     0       23     198.089     18.0365     0.1252     53     219.474     19.0241     0       24     196.405     14.2008     0     54     220.029     18.2827     -0.0747       25     196.985     16.4446     0     55     218.874     16.6868     0       26     197.24     16.1667     -0.1252     56     216.894     15.6998     -0.0102       27     197.225     16.0319     0     57     210.083     10.7181     0.0008       28     197.285     15.9908     0     58     216.244     23.1296     0       29     197.355     16.0061     0.0096     59     215.584     16.8071     0	17	194.245	16.7472	0	47	219.274	18.8057	0
20       195.195       17.3295       0       50       217.084       15.8526       0.0102         21       196.365       16.9369       0       51       210.265       10.7066       -0.0008         22       195.873       15.3693       0.0021       52       218.064       24.7841       0         23       198.089       18.0365       0.1252       53       219.474       19.0241       0         24       196.405       14.2008       0       54       220.029       18.2827       -0.0747         25       196.985       16.4446       0       55       218.874       16.6868       0         26       197.24       16.1667       -0.1252       56       216.894       15.6998       -0.0102         27       197.225       16.0319       0       57       210.083       10.7181       0.0008         28       197.285       15.9908       0       58       216.244       23.1296       0         29       197.355       16.0061       0.0096       59       215.584       16.8071       0	18	192.21	13.6553	0.1349	48	219.919	18.3572	0.0747
21       196.365       16.9369       0       51       210.265       10.7066       -0.0008         22       195.873       15.3693       0.0021       52       218.064       24.7841       0         23       198.089       18.0365       0.1252       53       219.474       19.0241       0         24       196.405       14.2008       0       54       220.029       18.2827       -0.0747         25       196.985       16.4446       0       55       218.874       16.6868       0         26       197.24       16.1667       -0.1252       56       216.894       15.6998       -0.0102         27       197.225       16.0319       0       57       210.083       10.7181       0.0008         28       197.285       15.9908       0       58       216.244       23.1296       0         29       197.355       16.0061       0.0096       59       215.584       16.8071       0	19	193.495	16.6867	0	49	218.914	16.69	0
22     195.873     15.3693     0.0021     52     218.064     24.7841     0       23     198.089     18.0365     0.1252     53     219.474     19.0241     0       24     196.405     14.2008     0     54     220.029     18.2827     -0.0747       25     196.985     16.4446     0     55     218.874     16.6868     0       26     197.24     16.1667     -0.1252     56     216.894     15.6998     -0.0102       27     197.225     16.0319     0     57     210.083     10.7181     0.0008       28     197.285     15.9908     0     58     216.244     23.1296     0       29     197.355     16.0061     0.0096     59     215.584     16.8071     0	20	195.195	17.3295	0	50	217.084	15.8526	0.0102
23     198.089     18.0365     0.1252     53     219.474     19.0241     0       24     196.405     14.2008     0     54     220.029     18.2827     -0.0747       25     196.985     16.4446     0     55     218.874     16.6868     0       26     197.24     16.1667     -0.1252     56     216.894     15.6998     -0.0102       27     197.225     16.0319     0     57     210.083     10.7181     0.0008       28     197.285     15.9908     0     58     216.244     23.1296     0       29     197.355     16.0061     0.0096     59     215.584     16.8071     0	21	196.365	16.9369	0	51	210.265	10.7066	-0.0008
24     196.405     14.2008     0     54     220.029     18.2827     -0.0747       25     196.985     16.4446     0     55     218.874     16.6868     0       26     197.24     16.1667     -0.1252     56     216.894     15.6998     -0.0102       27     197.225     16.0319     0     57     210.083     10.7181     0.0008       28     197.285     15.9908     0     58     216.244     23.1296     0       29     197.355     16.0061     0.0096     59     215.584     16.8071     0	22	195.873	15.3693	0.0021	52	218.064	24.7841	0
25     196.985     16.4446     0     55     218.874     16.6868     0       26     197.24     16.1667     -0.1252     56     216.894     15.6998     -0.0102       27     197.225     16.0319     0     57     210.083     10.7181     0.0008       28     197.285     15.9908     0     58     216.244     23.1296     0       29     197.355     16.0061     0.0096     59     215.584     16.8071     0	23	198.089	18.0365	0.1252	53	219.474	19.0241	0
26       197.24       16.1667       -0.1252       56       216.894       15.6998       -0.0102         27       197.225       16.0319       0       57       210.083       10.7181       0.0008         28       197.285       15.9908       0       58       216.244       23.1296       0         29       197.355       16.0061       0.0096       59       215.584       16.8071       0	24	196.405	14.2008	0	54	220.029	18.2827	-0.0747
27     197.225     16.0319     0     57     210.083     10.7181     0.0008       28     197.285     15.9908     0     58     216.244     23.1296     0       29     197.355     16.0061     0.0096     59     215.584     16.8071     0	25	196.985	16.4446	0		218.874	16.6868	0
28     197.285     15.9908     0     58     216.244     23.1296     0       29     197.355     16.0061     0.0096     59     215.584     16.8071     0	26	197.24	16.1667	-0.1252	56	216.894	15.6998	-0.0102
29 197.355 16.0061 0.0096 59 215.584 16.8071 0		197.225	16.0319	0	57	210.083	10.7181	0.0008
		197.285	15.9908	0		216.244	23.1296	0
<u>30 197.082 15.6599 0.3122 60 219.054 20.8838 0</u>	29	197.355	16.0061	0.0096	59	215.584	16.8071	0
	30	197.082	15.6599	0.3122	60	219.054	20.8838	0

#### 3.3. Comparing of Three Models Approach

Based on the discussion above, we can compare mean square errors (MSE), Errors ( $\varepsilon_t$ ) and plots for these three models approach, i.e., autoregressive, ARIMA and semiparametric (partly linear autoregressive) models as follows:

- (i). MSE of autoregressive, ARIMA, and semiparametric models are 11, 8.502 and 0.007083, respectively. We can see that MSE of semiparametric model approach is smaller than both autoregressive and ARIMA models approach.
- (ii). Errors ( $\varepsilon_t$ ) of both autoregressive and ARIMA models approach are not normal, but errors ( $\varepsilon_t$ ) of semiparametric model approach is normal as shown in Figure 14. However, these three models approach satisfy white noise condition.
- (iii). Plot between estimated values  $(\hat{y}_t)$  and observation values  $(y_t)$  for autoregressive, ARIMA and semiparametric models approach are given by Figure 15, Figure 16, and Figure 17, respectively. We can see that plot result of semiparametric model approach gives estimated values  $(\hat{y}_t)$  exactly close to observation values  $(y_t)$ . It is different from both autoregressive and ARIMA models approach.

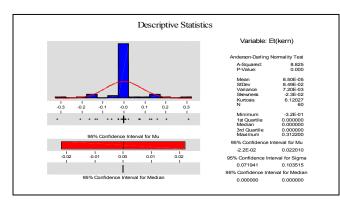
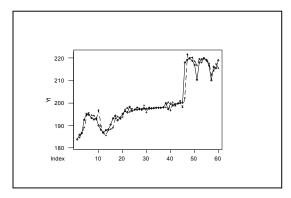
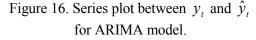


Figure 14. Residuals plot for semiparametric Model.

Figure 15. Series plot between  $y_i$ , and  $\hat{y}_i$ , for autoregressive model





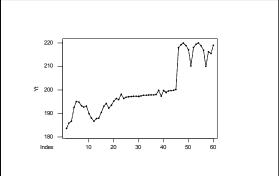


Figure 17. Series plot between  $y_t$  and  $\hat{y}_t$  for semiparametric model.

#### 4. Conclusion

Based on the discussion above, we known that using of semiparametric model approach for estimating a model of general consumer price index of Jember is better than both autoregressive and ARIMA models approach. We obtained an estimated model of general consumer price index of Jember as a semiparametric time series model which is called as partly linear autoregressive model as follows:

$$\hat{y}_{t} = 0.9192 y_{t-1} + \hat{g}_{T}(y_{t-2})$$
Where
$$\hat{g}_{T}(y_{t-2}) = \hat{g}_{1T}(y_{t-2}) - 0.9192 \hat{g}_{2T}(y_{t-2}),$$

$$\hat{g}_{1T}(y_{t-2}) = \sum_{s=3}^{T} W_{Ts}(y_{t-2}) y_{s},$$

$$\hat{g}_{2T}(y_{t-2}) = \sum_{s=3}^{T} W_{Ts}(y_{t-2}) y_{s-1},$$

$$W_{Ts}(y_{t-2}) = K((y_{t-2} - y_{s})h^{-1}) / \sum_{j=3}^{T} K((y_{t-2} - y_{j})h^{-1}) \text{ and}$$

$$K(y) = \frac{1}{\sqrt{2\pi}} e^{-\frac{1}{2}y^{2}}, \quad -\infty < y < \infty.$$

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